

An Improved Framework for Hybrid Energy Harvesting for Underwater Sensor Nodes and IoT

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Abstract- *Energy harvesting for sensor networks deployed at critical locations is an important research area now these days. Various types of energy harvesting techniques like solar, thermal, aquatic, wind energy harvesting systems are very popular in research community. This is found in the survey, that single energy harvesting technique is not enough for the wireless sensor network, specially when the nodes are deployed at critical areas like volcanoes, underwater, ocean, rivers etc. Finding energy solutions for perpetual, batteryless, and critical places where human intervention is not possible is the motivation of this paper. In this paper, a hybrid energy harvesting solution using solar, pressure, and thermal has been proposed. An optimized framework has been proposed, implemented, and analyzed for underwater sensor network application. A mechanical and an electrical schematic has been designed, implemented, and realized. The physical parameters of solar, thermal, and piezoelectrical transducers has been analyzed along with mathematical equations to find the best possible solutions for the optimized framework. The model is theoretically implemented and investigated, and this is found that 13.66KJ of energy can be extracted in 24Hrs from the proposed design which guarantees a perpetual lifetime of sensor node.*

Indexed Terms- *Energy harvesting, Sensor network, underwater sensor network, Solar, thermal, piezoelectric.*

I. INTRODUCTION

Sensor technologies have revolutionized, and we have advanced enough to deploy sensor technologies in different kinds of remote environments. More than 3/4th of the earth's total surface is covered with water (majorly rivers, oceans and seas) and it has become a necessity to monitor these environments to get informative and utilizable data [1]. With the development of new technologies, we have new ways to sense marine environments [2,3]. There are a wide range of applications [4-12] of underwater sensing such as water quality monitoring, recording the

quantity of pollutants and toxins, marine surveillance, aquaculture, climate recording, prediction of natural disasters, study and survey of marine environments and other commercial applications such as oil industries etc.

Along with the several problems in deploying sensor nodes underwater one major problem is the energy needs of the sensors [13]. Since, these sensors are deployed in remote areas underwater which might not be easily accessible, it is very difficult to maintain and replace batteries of these sensor nodes. Depleted batteries would then interfere with the proper functioning of the sensors and would compromise with its performance [14-19].

Hence, we come up with a hybrid model of harvesting energy easily and efficiently which would require very little maintenance. These harvesting techniques would replace the batteries, be pollution free and harmless to aquatic life [20, 21]. They would not compromise with the performance of the sensors and networks as they are inexhaustible. We are converting waste physical energy in the environment into usable electrical energy [22]. Relying on one source of energy wouldn't be wise as it may be possible that it's not available at some point of time [23]. Hence, we came up with a model that utilizes three different sources of energy as one might not be enough to satisfy the energy needs of the sensor node for a perpetual lifetime [24].

We propose to utilize solar, thermal energies and piezoelectricity in the same hybrid model. Solar energy can be easily generated using PV (Photovoltaic) cells. However, it is not possible to harness solar energy during night-time. For that purpose, we have a thermal electric generator (TEG) installed in our model. Harnessing piezoelectricity from the mechanical stress applied by water molecules would ensure a continuous supply of power to the sensor nodes as it would be always available in the oceans/seas.

Further, the paper is configured as follows. Section I contains the introduction of the energy harvesting techniques; Section II is associated with literature review and related work. Section III, is related to proposed framework of hybrid energy harvesting modules. Section IV, shows the parameters related to solar, thermal and piezoelectric energy transducers. Section V having the simulation and results. And finally, conclusion of the paper has been drawn in section VI.

II. RELATED WORK

According to [25], the efficiency of Si cells can be improved by the technique of Multi Junction Solar Cells. These cells contain more than one layer of PV cells with many different energy band gaps attached together and this results in a better usage of the solar spectrum.

In [26], the researchers have turned a wearable jacket to an energy harvesting system. It was observed that the system harvested 0.9mW of energy during sitting posture. This technology had 16 PV Cells, 12TEGs and 5 power management Integrated Circuits (ICs). This model is capable of powering 2 AAA NiMH batteries in series. The solar and thermal harvesting chips used were TI BQ25504. By using a PV Cell on top of a TEG the authors observed a 4-5% gain in efficiency.

In [27], the authors came up with the idea of using a DC-DC boost converter in a thermal energy harvester, which produced usable electrical energy from waste thermal energy. This thermal energy was used to power Wireless Sensor Nodes(WSN) to improve their working lifetime.

In [28], a macro level thermal energy harvesting technique was proposed which was inexpensive but the temperature difference between both sides created a major issue. A minimum of 100C of temperature difference must be there between both sides of the TEG for an efficiently working system.

Authors in [29], proposed a TEG model to harvest thermal energy that generated several joules of energy. It was suggested that better heat sinks and larger supercapacitors would solve the problem of the less

temperature difference between 2 sides of the TEG. In [30], a simulated model was presented which controlled the DC-DC converter duty cycle to obtain maximum TEG Power.

In [31], a system to supply power to low power sensors in aircrafts using TEG was presented. In which TEG's open circuit voltage is measured automatically as part of a power management technique and the maximum harvested power is recorded. In [16], Alper and Ghislain experimentally investigated and proved the concept of piezo hydroelasticity for underwater thrust and power generation, they found out that The average power requirement for generating a mean thrust of 19 mN at 6 Hz is measured as 120 mW. A 50.8mm×25.4mm×0.017 mm thin film battery (2.5 mAh, 4 V) can provide this power for 5 min.

In [14], the authors examined different power management schemes and energy harvesters with an objective of underwater node lifetime improvement. The authors used ambient energy present in water flow and acoustic waves and converted them to electrical energy using hydrokinetic turbine, piezoelectric cantilever, and hydrophone to supply power to nodes.

III. PROPOSED FRAMEWORK

To run the Underwater Sensor Network (UWSN) nodes continuously, we have used techniques to harvest power from inexhaustible resources. Three sources of energy in a single system to make it reliable and efficient has been used. Solar cells are placed to harvest solar energy at the topmost layer of our hybrid model, it is followed by an Aluminum Plate and a water chamber. At the bottom, a Lead Zirconate Titanate (PZT) crystal which harvests piezoelectricity has been used. The whole model will be placed on a buoy to keep it over the water surface with just PZT crystal exposed to the water. An electrical schematic has been also with passive components to channelize the stored energy in proper way. Following are in detail discussion about the mechanical and electrical schematic.

a. Mechanical Schematic

Figure 1 shows the mechanical schematic. The topmost layer, i.e., Photovoltaic (PV) Cells collect photons from the sunlight and subsequently convert it

into electrical energy. An Aluminum plate is placed just below the solar cells. Aluminum is a great conductor of heat, so it gets heated in the daytime. Beneath that is a Thermoelectric Generator (TEG) which works on peltier's effect and convert the gradient of thermal energy into electrical energy. A chamber which contains the Phase Change Material (PCM) i.e. water is present beneath the TEG. After that a PZT crystal which is exposed to water is present, this PZT crystal generates Piezoelectricity, converting the mechanical stress generated by water molecules into usable electricity. This is the last layer of proposed mechanical schematic model.

Phase change material (PCM) is a material used in thermal electric generators which store/dissipate energy whenever there is a change in phase, for eg: gaseous to liquid. This heat is absorbed and stored and can be used after some time. During the day, water (PCM) is cooler than the Aluminum plate and heat flows from Al to Water and the TEG generates electricity utilising this flow of heat. The opposite happens during the nighttime when the Al plate is cooler than water and there is heat flow from Water to Al, the TEG utilizes this flow of heat as well and generates usable electricity. The PZT crystal experiences stress from the water molecules beneath it, this stress polarizes the ferroelectric crystal and generates utilizable electricity.

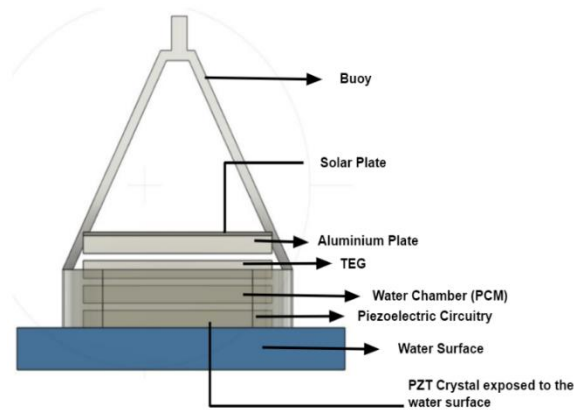


Figure 1: Mechanical Schematic

The buoy keeps the arrangement on the surface of water preventing it from sinking. It has been created such that there is access to air for the water chamber. The solar plate generates solar energy. The Al plate and water chamber are important for the functioning of the TEG. Below that is the required circuitry needed

to harness piezoelectricity (which will be discussed in the later sections). The PZT crystal is placed beneath this arrangement.

b. Electrical Schematic

The electrical schematic as proposed is given in figure 2. The given circuit shows the implementation of our model electrically. We use a buck-boost converter IC i.e REES52 to convert the voltage to 5.5V to charge the capacitor. Between the output of the buck-boost converter and the capacitor is a MOSFET acting as a switch. This switch will be closed until the capacitor has 4.86V or less than that; as soon as it has a greater voltage than 4.86V the switch will open and prevent overcharging or overflow of current. This voltage comparison is done using an Op-Amp LM311.

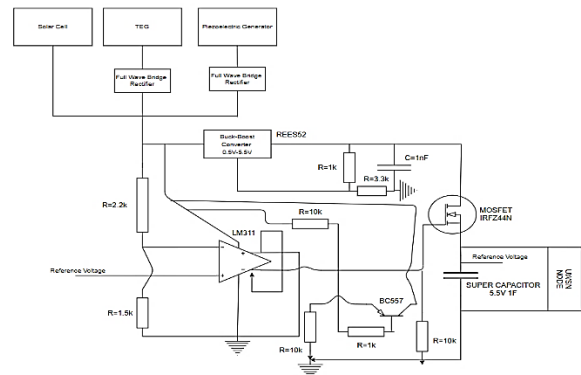


Figure-2: Electrical Schematic (All values of resistances are in Ω)

A full wave bridge rectifier has been used with the TEG to ensure supply of current in a single direction. A voltage divider circuit has been used with the output of the converter to regulate the voltage exactly at 5.5V. We have used an LM311 comparator IC to compare the voltage values of the supercapacitor and the input voltage. This input voltage is supplied to pin number 2 of the op-amp using a voltage divider circuit. The resistors 2.2k and 1.5k drop a voltage of 4.86V from the input. This 4.86 volt is compared with ref voltage (voltage of capacitor) which is connected to pin 3. When the ref voltage is smaller than 4.86V the output pin 7 will go high and the input voltage with the pull-up 10k resistor. This voltage will then be used to operate the MOSFET. The IRFZ44N MOSFET is used to connect the super capacitor and the charging voltage which is manipulated by the signal from the op-amp. When the op-amp goes high it supplies the input voltage on pin 7 which turns on the MOSFET through

its base pin. The same happens when the op-amp goes low (0V), the MOSFET will be opened. We also have a PNP transistor BC557 which prevents the extra flow of current reducing the wastage and loss of power in the circuit.

The capacitor is connected directly to the UWSN node, this node draws voltage from the capacitor as per its needs and the sensor runs continuously without any issue. Neither the performance nor the efficiency of the sensor is compromised.

IV. PARAMETERS

Parameters of TEG, PV cell and PZT has been discussed in this section. Parameters may help us to design the optimal solution of the hybrid energy harvesting. The details of parameters are as follows:

a. TEG Parameters

The parameters which affect the working of TEGs are Seebeck Coefficient (greater the value of Seebeck Coefficient greater is the conversion of thermal energy to electrical energy), thermal conductivity (measure of a material's ability to conduct heat), load and internal resistances and heat transfer. Table 1 shows the parameters of Bismuth Telluride (Be_2Te_3). More details of the parameters have been considered from [28]. Readers may follow the [28] for more details

Table 1: Values of Parameters of TEG for Be_2Te_3

S.No.	Parameter	Notation	Value
1.	Thermal conductivity of Ceramic Substrate	λ_{Sub}	180W/mK
2.	Thermal conductivity of Thermocouple	λ	1.5W/mK
3.	Substrate Thickness	L_{Sub}	0.9mm
4.	Antimony Telluride (p-type) Seebeck Coefficient	α_p	185 μ V/ $^{\circ}$ K

5.	Bismuth Telluride (p-type) Seebeck Coefficient	α_n	- 228 μ V/ $^{\circ}$ K
6.	Electrical conductivity of n-type	ρ_n	12.6 $\mu\Omega$ m
7.	Electrical conductivity of p-type	ρ_p	12.6 $\mu\Omega$ m
8.	Length of thermal element	L	1.6mm
9.	Total number of thermocouples	N	127
10.	Thermal conductivity of n-type	σ_n	1.8W/mK
11.	Thermal conductivity of p-type	σ_p	1.3W/mK

Figure of merit of TEG is directly proportional to the square of the Seebeck Coefficient. The material's ability to generate Thermal Energy is dependent on the figure of merit. Hence for a high conversion rate of thermal energy to electrical energy, a high value of Figure of merit (ZT) is needed. Eq. 1 below gives the value of ZT

$$ZT = \left(\frac{(\alpha_n - \alpha_p)^2}{\rho_n \sigma_n + \rho_p \sigma_p} \right) T \tag{1}$$

Here T is the average temperature of the TEG module. The eq. 2 below gives the efficiency of the TEG-

$$\eta_{TEG} = \frac{\Delta T (\sqrt{1+ZT} - 1)}{T_h (\sqrt{1+ZT} + \frac{T_c}{T_h})} \tag{2}$$

The efficiency of the TEG Module is directly proportional to the temperature difference ΔT and ZT.

b. Solar Cells Parameters

Photovoltaic (PV) Cells called solar cells harvest electrical energy from solar energy. Photons from the sun strike the semiconductor layer of the solar cells and generate electron-hole pairs; these free electrons then flow in the external circuit as electric current.

Solar panels, which are a combination of many solar cells, are used as they generate a higher voltage. Each Si solar cell can produce around 0.5-0.6volts. Following are the equations in support of PV cells.

$$I = N_p I_{ph} - I_d - I_{Rsh} \tag{3}$$

$$I_{ph} = [I_{sc} + k_i(T - T_{ref})] \frac{G}{G_{ref}} \tag{4}$$

$$I_D = I_S [\exp(\frac{qV_d}{nKT} - 1)] = I_S [\exp(\frac{q(V + IR_S)}{nNSCKT} - 1)] N_P \tag{5}$$

$$I_S = I_{rs} (\frac{T}{T_n})^3 \exp[\frac{qE_{go}(1/T_n - 1/T)}{nK}] \tag{6}$$

$$I_{sh} = (\frac{V + IR_S}{R_{sh}}) \tag{7}$$

$$V_T = \frac{KT_{op}}{q} \tag{8}$$

$$V_{OC} = V_t \ln(\frac{I_{ph}}{I_S}) \tag{9}$$

$$\eta = \frac{V_{oc} I_{sc} FF}{P_{in}} = \frac{V_{mpp} I_{mpp}}{P_{in}} \tag{10}$$

$$FF = \frac{Max\ Power}{V_{oc} I_{sc}} \tag{11}$$

c. PCM (Phase Change Material)

PCM is a material that stores energy when there is a change in state at the Phase Change Temperature (PCT), this stored energy is later radiated and utilized efficiently. For the efficient performance of the TEG, the PCM plays an important role hence it must be chosen very carefully. Here we choose water as the suitable PCM because it has high volumetric latent heat storage capacity and it is easily available at a low cost., It has sharp melting point, high thermal conductivity, high heat of fusion of approximately 333.6kJ/kg, non-flammable, chemical stability, completely reversible freeze/melt cycle, no degradation after many freeze/melts cycle, non-corrosiveness, non-toxic and non-explosive material. Apart from this it also has a high energy of phase change, high latent heat, and high specific heat. Higher thermal conductivity leads to a greater ease of transfer of heat from the TEG module. The TEG’s operating temperature conditions are also satisfied if water is used as the PCM.

d. Piezoelectric Generator

The Piezoelectric generator harvests energy by converting the mechanical stress/vibrations to usable electrical energy. The performance and the conversion rate depend on the piezoelectric material used and many other factors discussed below-

Density, piezoelectric coefficients, relative permittivity, electromechanical coupling factor and

mechanical quality factor. We’re using PZT-5H which is DOD Type VI, Lead-Zirconate Titanate it has the following properties -Very high strain (charge) constants, permittivity, and coupling constants, Modest Curie temperature restricts its temperature range and thermal stability, low mechanical quality factor, high charge output useful for sensing devices and generator elements, high strain output useful for large displacements at lower voltages, used for sensing (receivers, knock, hydrophones, pick-ups, medical diagnostics), used for actuators (valves, positioning, fans, tilters). The values of the various parameters have been given below for PZT-5H

Piezoelectric coefficients(d) in pC/N : d₁₅=741, d₃₁=-274, d₃₃=593; Relative Permittivity (ε_r) : ε₁₁=3130, ε₃₃=3400; Electromechanical Coupling factor (k): k₁₅=0.68, k₃₁=0.39, k₃₃=0.75; Quality factor=65; Density=7600 kg/m³. PZT-5H has a high Curie Temperature hence providing a high thermal stability, The crystal structure of a material changes at the Curie temperature from piezoelectric (non-symmetrical) to a non-piezoelectric (symmetrical) form, and the material loses its piezoelectric properties. This phase change is accompanied by a peak in the dielectric constant at that temperature. The Curie temperature, T_c, is expressed in degrees Celsius. For PZT-5H T_c is 120°C which can be further increased by adding silver to the ceramic crystal. The piezoelectric coefficients (d₃₃, d₃₁, d₁₅ etc.) measure the strain which has been induced by an exerted voltage (in meters per volt). High values of dij coefficients show larger displacements which are desperately needed for motoring transducer devices. The coefficient d₃₃ measures deformation in the same direction (polarization axis) as the induced potential, whereas d₃₁ describes the response when the force is applied perpendicularly to the polarization axis. The d₁₅ coefficient measures the response when the applied mechanical stress is because of shear deformation. Relative permittivity (ε_r) is the ratio between the value of absolute permittivity of the piezoelectric material, ε, to the value of vacuum permittivity, ε₀. The electromechanical coupling factor k tells us the effectiveness with which a piezoelectric material converts electrical energy into mechanical energy, or converts mechanical energy into electrical energy. The first subscript to k denotes the direction along which the electrodes are applied; the second denotes the

direction along which the mechanical energy is applied, or generated. The mechanical quality factor Qm is a major high-power attribute of piezoelectric ceramic materials. It is the inverse of the mechanical loss tan φ. Below is a table(3) which gives the values and meanings of all the notations used

Table-3: Notations used for Piezoelectric Generator with meanings and values

Notation	Meaning	Value for PZT-5H
K ^T	Relative Dielectric Constant when there are no external forces	1700
k ₃₁	Electromechanical Coupling Factor/Coefficient(applied stress is in 3 directions)	0.35
k ₃₃	Electromechanical Coupling Factor/Coefficient(applied stress around 2 axis)	0.69
T _C	Curie Temperature	120°C
ρ	Density	7600kg/m ³
d ₃₁	Piezoelectric Charge Coefficient(applied stress in 3 directions and electrodes along 1 axis)	1.8e-10 m/V
d ₃₃	Piezoelectric Charge Coefficient(applied stress in 3 directions and electrodes perpendicular to 3 axes)	3.6e-10 m/V
g ₃₁	Piezoelectric Voltage Coefficient(Applied stress in 1 direction and electrodes perpendicular to 3 axis)	0.011 Vm/N
g ₃₃	Piezoelectric Voltage Coefficient(applied stress in 3 directions and electrodes perpendicular to 3 axes)	0.025 Vm/N
Y	Young's Modulus	63GPa
s	Compliance	0.015X10 ⁻⁹ Pa ⁻¹

The following equations (12) give us the formulae of all the parameters discussed above-

$$K^T = \frac{C_0 h}{\epsilon_0 A} \tag{12}$$

Here K^T is the relative dielectric constant of the material, ε₀ is the relative permittivity of free space(8.854 X 10⁻¹² F/m), h is the distance between electrodes in metres, A is the area of electrodes in m² and C₀ is the capacitance at 1kHz

$$Q_M = \frac{1}{2\pi F_r Z_m C_0} \left(\frac{F_a^2}{F_a^2 F_r^2} \right) \tag{13}$$

Here F_r is the resonance frequency, F_a is the anti resonance frequency, Z_m is the impedance at F_r and C₀ is static capacitance in Farad

$$k = \sqrt{\frac{\text{Electrical energy stored}}{\text{Mechanical Energy Applied}}}$$

$$1 + k_p^2 = \frac{(1 - \sigma^E) J_1[\eta_1(1 + \frac{\Delta F}{F_r})] - \eta_1(1 + \frac{\Delta F}{F_r}) J_0[\eta_1(1 + \frac{\Delta F}{F_r})]}{(1 + \sigma^E) J_1[\eta_1(1 + \frac{\Delta F}{F_r})]} \tag{14}$$

Here k_p is the electromechanical coupling factor, J₀=Bessel function of the first kind and zero order, J₁=Bessel Function of the first kind and first order, σ^E is the Poisson's Ratio, η₁ is the lowest positive root of (1 + σ^E)J₁η = ηJ₀(η)

It has been assumed that for Lead Zirconate Titanate, σ^E = 0.31 and η₁ = 2.05

And ΔF = F_a - F_r (Hz).

Defining one more parameter, x which is given as x = $\frac{\Delta F}{F_r}$

$$k_{33}^2 = \frac{\pi}{1+x} \tan\left(\frac{\pi x}{1+x}\right) \tag{15}$$

$$\frac{k_{31}^2}{1+k_{31}^2} = \frac{\pi}{2} (1+x) \tan\left(\frac{\pi}{2} x\right) \tag{16}$$

Another parameter called effective coupling coefficient of an arbitrary resonator (k_{eff}) is given as-

$$k_{eff}^2 = \frac{F^2 a - F^2 r}{F^2 r} \tag{19}$$

Piezoelectric charge coefficient(d) is the ratio between electric charge generated per unit Applied Stress expressed in C/N

$$d = \frac{\text{charge density (open circuit)}}{\text{Applied stress}} \tag{20}$$

$$d = k\sqrt{\epsilon_0 k^T s^E} \tag{21}$$

Here s is the compliance (10⁻¹² m²/N), rest of the notations have been discussed above

Piezoelectric Voltage Coefficient(g) is the ratio of electric field produced over mechanical stress applied expressed as Vm/N

$$g = \frac{d}{\epsilon} \tag{22}$$

d is the charge density and ϵ is the relative permittivity

$$s = \frac{1}{Y} \tag{23}$$

$$s = \frac{\text{strain}}{\text{stress}} \tag{24}$$

$$s = \frac{l^2}{\rho v^2 N} \tag{25}$$

Here Y is the Young's Modulus of elasticity and l is the length ρ is the density and v is the sonic velocity ($v=2\pi fl$)

$$\text{stress} = \frac{\text{Mechanical Force Applied}}{\text{Area}} \tag{26}$$

$$\text{strain} = \frac{\text{change in length of the material}}{\text{initial length}} \tag{27}$$

$$g = \frac{\text{Field Developed}}{\text{Applied Mechanical Stress}} \tag{28}$$

The figure(4) below shows the electrical schematic of the piezoelectric generator

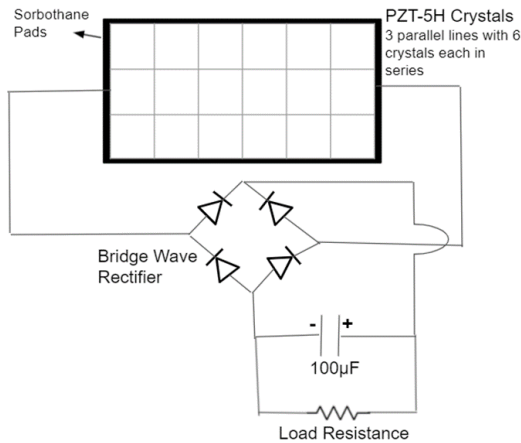


Figure-4: Electrical Schematic of Piezoelectric Generator

A total of 18 small PZT crystals are used with 6 placed in series in order to increase the generated voltage and 3 such parallel lines are used in order to maximise the output current as the total current would be the sum of the current generated by all the individual lines. Next is a full wave bridge rectifier so that the current flows in a single direction only. The output of the rectifier is fed to the capacitor. This capacitor stores the charge and supplies it to the load resistance as per it is needed. The PZT crystals are kept in their place firmly by sorbothane pads, these pads also protect the crystals from any damage. These pads also increase the amount of voltage generated marginally as they also produce mechanical stress on the PZT crystals.

Assuming the ocean/sea current speed to be 1.7778m/s [32] and if water molecules come to rest after colliding with the PZT layer. We are using crystals of dimensions 8cms length, 6cms width and 3cms height. Since there are 18 such crystals, the total area of the cross section would be 864 cm². Assuming water molecules at a depth of 5 metres can reach and collide with the PZT crystals and density of seawater is 1023.6kg/m³. So the stress generated by water molecules on the PZT crystals would be approximately 3233.24265 N/m². Stress on each crystal is 179.624591667 N/m².

Now voltage generated by each crystal can be found out using equation(22), putting the values(g for PZT is 0.025Vm/N) it comes out to be 0.269436Volts. Since there are 6 such crystals in series therefore total voltage generated 1.617 Volts.

CONCLUSION

The study involves the centrifugation of cane juice. The juice is subjected to centrifugation directly after milling of the cane. This treatment has been thought of particularly to clarify juices by removing the suspended particles, viz. silica, organic salts, etc. along with mud. In this paper the design pattern of the centrifuge has been shown. The effective factors such as removal of suspended particles, clarity and ICUMSA colour of the centrifuged juice has shown by the table and graph.

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