

Performance Optimization of Optical Devices Using Multicore

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Abstract— *Integrated multicore structures are good candidates to improve the performance of active optical devices [1]. We are working on the characterization of these fabricated structures by femtosecond laser writing [2]. The two modal characterization techniques implemented by our group are presented.*

Indexed Terms— *multicore, power distribution, computer-generated holograms*

I. INTRODUCTION

Control over modal composition is essential for the optimized design of multicore active embedded structures. In the literature there are two experimental techniques of modal characterization for this type of structures: [1][2][3] the recording with a camera of the transverse power distributions at the output of the structure and its treatment by computer using imaging techniques and [4][5][6] the use of Holographic Optical Elements (HOEs) to spatially separate in real time the components of each mode [7].

II. CHARACTERIZATION BY POWER DISTRIBUTION

The number of modes allowed and the transverse power distribution of each one are characteristic properties of each guide and the working wavelength. We have the necessary software to calculate all this, given the transversal distribution of the refractive index (RSoft CAD) [2][3][7][8]. On the other hand, the distribution of the total power coupled to the guide between its different modes depends on how it is excited.

Figure 1 shows the experimental set-up that allows the excitation of the guide to be varied and its transversal power distribution to be measured. Its location, within the substrate on which it has been recorded, is possible

thanks to a microscope [9][10]. This also facilitates the optimization of the confrontation between the entrance of the guide and the optical fiber that provides the light. To optimize and ensure the stability of the assembly, the positions of the fiber and the guide are regulated with piezoelectric controllable micro-positioners [11]. Any lateral displacement between fiber and guide obviously modifies the total coupled power, but also the proportion of power carried by each mode. As a result, the transverse power distribution changes as the fiber-guide engagement is decentered [3][4][12][13].

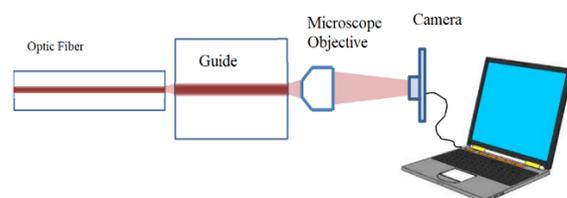


Fig. 1 Experimental setup to measure the transverse distribution of power at the output of a guide.

Next to the other end of this, a microscope objective is placed that forms the image of the exit face of the guide in a CCD camera (Bobcat 320 by Xenics). The magnification provided by the optical system, adjustable by moving the objective relative to the guide output, easily reaches a factor of 200x. Considering that the size of the pixels of the camera is 20 μm , a resolution of up 0.1 μm to the transverse distribution of output power of the guide can be available[15]. The proportion of the total power carried by each mode is determined by adjusting the image obtained to a sum weighted cross-sectional distributions characteristics of each mode, previously calculated using the aforementioned software[16].

III. CHARACTERIZATION BY CGH

Another way of knowing the modal distribution at the exit of the guide is through the use of computer-

generated holograms (CGH) [3][4][12][17]. These holograms can be digitally calculated and recorded in a spatial light modulator (SLM) device. When a hologram is recorded with the interference of a reference plane wave, R, and an object wave, O_n , formed by the complex amplitude distribution of one of the modes, n, at the output of the guide, the transmittance of the holographic element, $t(x,y)$, is proportional to the intensity of said interference.

$$t(x, y) = [O_n(x, y) + R(x, y)][O_n^*(x, y) + R^*(x, y)] = O_n O_n^* + R R^* + O_n R^* + O_n^* R$$

The last two addends have information on both the amplitude and the phase of both waves. If we digitally record the fourth addend in a phase SLM, when the SLM is illuminated with the power distribution at the guide output, $\sum_n c_n O_n$, at the output of the SLM there will be a plane wave $c_n R$, in the direction of the reference wave R, whose intensity is proportional to the intensity of the modo n.

In the SLM, the interference of each of the modes can be recorded with a reference wave R tilted at a different angle for each mode. In this way, at the output of the SLM we will be able to identify the contribution of each mode through the diffracted waves, their intensity ratio being proportional to that of the different modes at the output of the guide. In order to achieve the same amplitude distribution on the modulator as at the output of the guide, a system $4f$ made up of two lenses (L1 and L2) has been included in the assembly. The beam diffracted by the holographic element recorded in the SLM propagates in a different direction and its intensity is collected in a detector with the help of a lens (L3) (Figure 2).

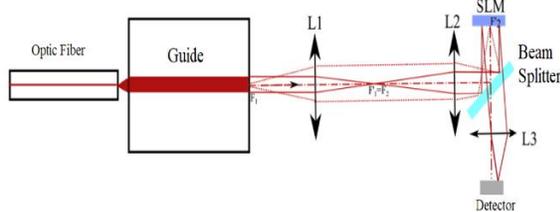


Fig. 2: Setup for mode recognition with a holographic optical element

CONCLUSION

The modal characterization of multicore integrated guides by means of two different experimental methods allows to test their validity and contributes to the optimized design of these structures.

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